

Sliding Pressure Study - Beebee Unit 12

Craig Litt
Rochester Gas & Electric Corporation

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Beebee Unit 12

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Station Engineer Performance
Rochester Gas and Electric Corporation

ABSTRACT

A study was done at Rochester Gas and Electric Corporation utilizing PEPSE to evaluate the heat rate benefit of sliding pressure operation on a 35 year old, 85 megawatt gross, single reheat unit. The results of this study were included in a response to a Public Service Commission concern regarding the benefit of sliding pressure operation. The PEPSE model used was the Benchmark model modified to fix the flow passing capability of the throttle valve to four valves open. The benefit was calculated to be 300 BTU/kwh. Model development, results and difficulties encountered in this analysis are discussed.

INTRODUCTION

"R.G.&E. Unit 12 is a General Electric 75000 kw machine with a tandem compound, double flow reheat turbine and a hydrogen cooled generator. Steam for the turbine is supplied by a Combustion Engineering controlled circulation, reheat type steam generator. The unit is designed for a flow of 560000 lbs/hr at 1825 psig and 1055 deg F at the superheater outlet and a reheat flow of 441000 lbs/hr at 1005 deg F. There is one constant speed and one variable speed boiler feed pump."¹

A PEPSE turbine model was used to evaluate the benefit of variable pressure operation. The model was developed by using the original vendor heat balances and PEPSE VER53 G.E. turbine components. The model was translated to General Turbine components that matched the PEPSE output from the G.E. components. This enabled the use of Special Option 6 (Automatic Test Data Reduction). Schedules on stage efficiency and shaper "constants" were added to allow the model to reflect loads from guarantee down to 25% load. The lowest heat balance was not able to be matched as it defies thermodynamic laws. Leakoffs from the valve stem and shaft packing combine and are piped to the lowest heater extraction line. The energy stated on the heat balance suggests the heater becomes an energy source. The hotwell makeup flow was made zero.

Cases were run first with the direct drive feedpump removed

¹ Gilbert Associates "Engineering Data For Beebee Station Unit 12" Architect Engineers

from service at throttle flows less than 69.5% guarantee flow, then second with the hydraulic coupling pump removed from service over the same load range. Schedules based on pump curves supplied with the thermal kit were included in the model to simulate sliding pump pressure. This gave a comparison of the cost/benefit of running the direct drive vs. variable speed pump. The results plotted on Figure 1 are Heat Rate vs. Mw Output with each pump out to show the effect of pump drive on turbine heat rate. There is a 200 BTU/kW savings at minimum load using the hydraulic coupling pump vs the direct drive pump. These savings resulted only from the difference in predicted pump performance as given in the thermal kit.

The next set of cases run utilized PEPSE Special Option 1 (Performance Based on Reference Conditions) to determine the flow passing capability of the throttle valve. The variable TFIRST (first admission equivalent throttle flow ratio) value on the throttle valve card was lowered to 0.1. This negated any throttling losses PEPSE would calculate at low inlet flows. Inlet pressure was reduced in 100 psi decrements to develop a Mw Output vs. Inlet Pressure curve. The results displayed in Figure 2 show two operating regimes. The continuously increasing line is the result of full sliding pressure operation. The second line is a hybrid sliding pressure operation. Since G.E. suggests a 100 psi, 100 deg F per hour ramp rate to return to design inlet conditions, operation below 800 psia would not be recommended unless the unit was on spinning reserve. This is indicated on the Benchmark vs. Sliding Pressure graph where the 'Full Sld' mode curve intersects with the 4 Valves Hybrid mode curve (Figure 4). For loads below this point, admission valves should be used.

Another set of runs was made with the First Stage Efficiency fixed to the valves wide open value. As expected, the results showed a marked decrease in Heat Rate. The shape of the curve (as shown in Figure 3) is parallel to the results of a set of runs made allowing the governing stage efficiency to vary as in the benchmark case. The savings of operating in this hybrid mode were calculated to be nearly 300 BTU/kWh. This is within the range of savings reported by New York downstate utilities in discussions following a New York Power Pool subcommittee meeting.

The methodology used to analyze sliding pressure is predicated on the assumption that the PEPSE model will accurately predict heat rates below the lowest accurate heat balance. This may not be valid because of the use of inaccurate vendor heat balances to create the benchmark models. Turbines built pre-1960 do not match the GE Procedure 20007C. The heat balances, when plotted on a Mollier diagram, do not yield parallel expansion lines as predicted. This is why shapers were used to modify the expansion lines to fit best available documentation. The heat balances available to model this turbine do not have the first stage bowl state conditions indicated. This caused the assumption of varying stage efficiency to be used in the benchmark to match valve stem leakoff enthalpy. The stage efficiency should be constant and the throttle valves should show the throttling effects. The effects of these omissions are negligible at full load, and exaggerated at low loads.

The PEPSE input deck is in Appendix A along with a schematic heat balance.

CONCLUSIONS

A hybrid mode of operation for loads below a conservative value of 30 MwG would yield a savings . The throttle pressure should not go below 800 psia. This is the value shown on the Benchmark vs. Sliding Pressure graph where the Full Arc mode curve intersects with the 4 Valves Hybrid mode curve. For loads below this point, admission valves should be used. A test of actual results could be developed to quantify savings and unit response.

SUMMARY

A series of PEPSE cases were run to evaluate the benefits of sliding pressure operation on an 85 MwG G.E. turbine. Modeling techniques used included the use of Special Option 1 and schedules developed from the thermal kit supplied by the A.E.. Problems and assumptions made in this analysis include vendor heat balance inaccuracies, omissions of first stage design conditions and generic performance curves. Savings were calculated to be 300 BTU/kwh.

ACKNOWLEDGEMENTS

The author would like to acknowledge the following people for their time and patience:

Steve Bonner of Oklahoma Gas and Electric

Don Fleming and Gene Minner of NUS/EI

IHRAS members from ConEd, LILCO, and Central Hudson Utilities

Steve Klein of Stoller Company.

HEAT RATE vs. LOAD VARIABLE vs. DIRECT DRIVE

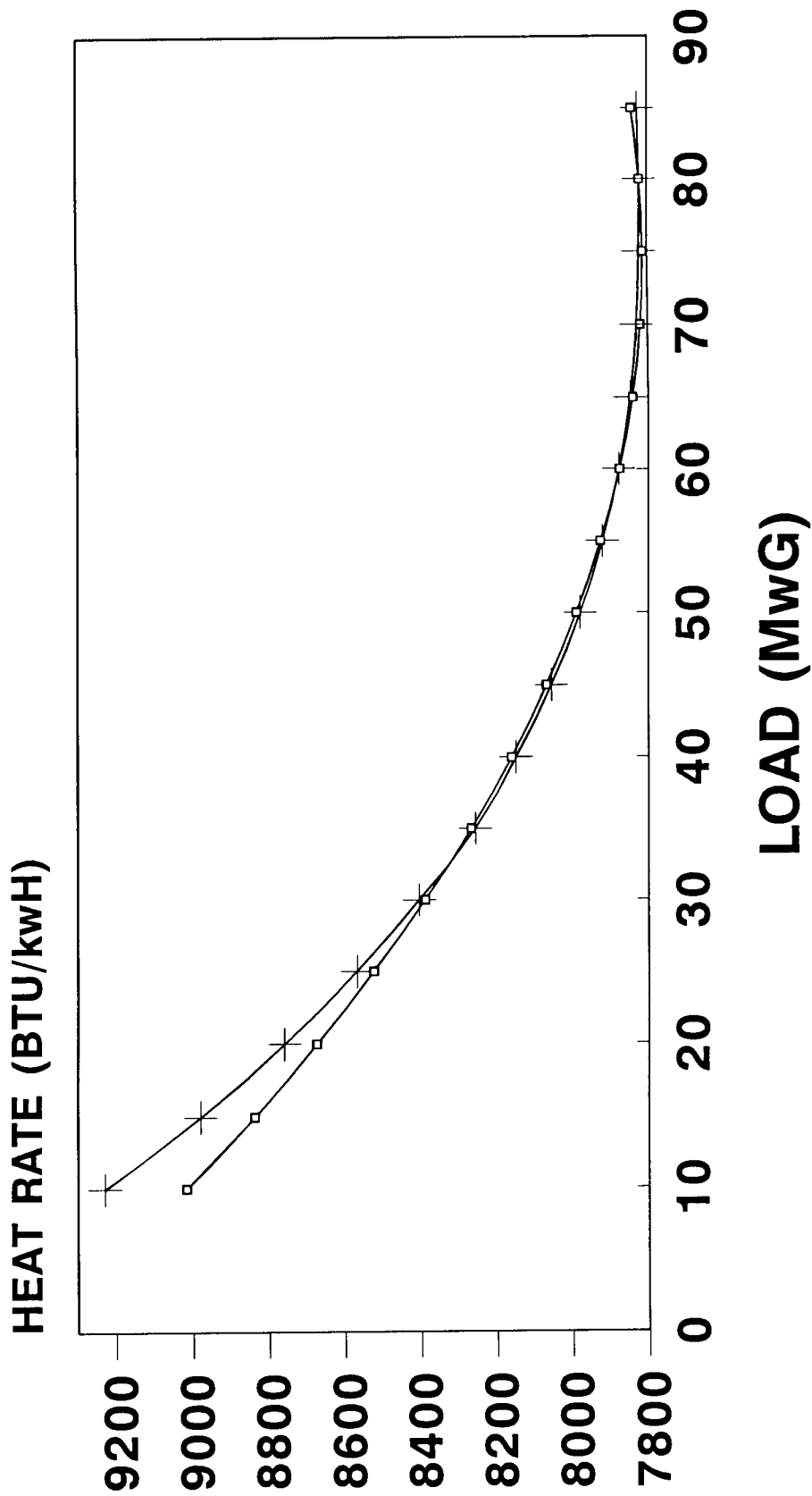


FIGURE 1

□ VARIABLE SPEED + DIRECT DRIVE

UNIT 12

THROTTLE PRESSURE vs. LOAD

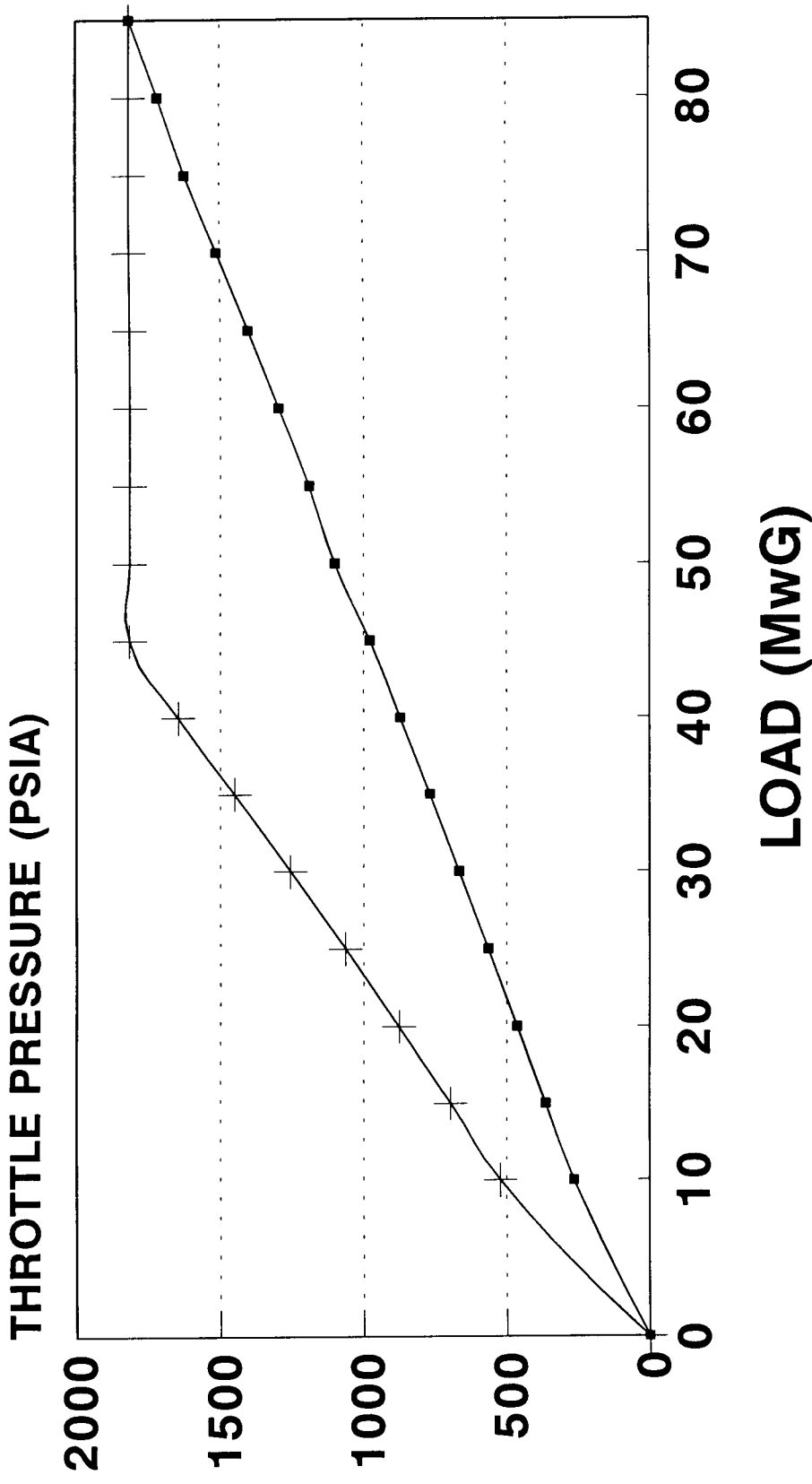


FIGURE 2

—■— FULL ARC ADMISSION —+— 4 VALVE HYBRID

UNIT 12 HEAT RATE BENCHMARK vs. 4 VALVE HYBRID

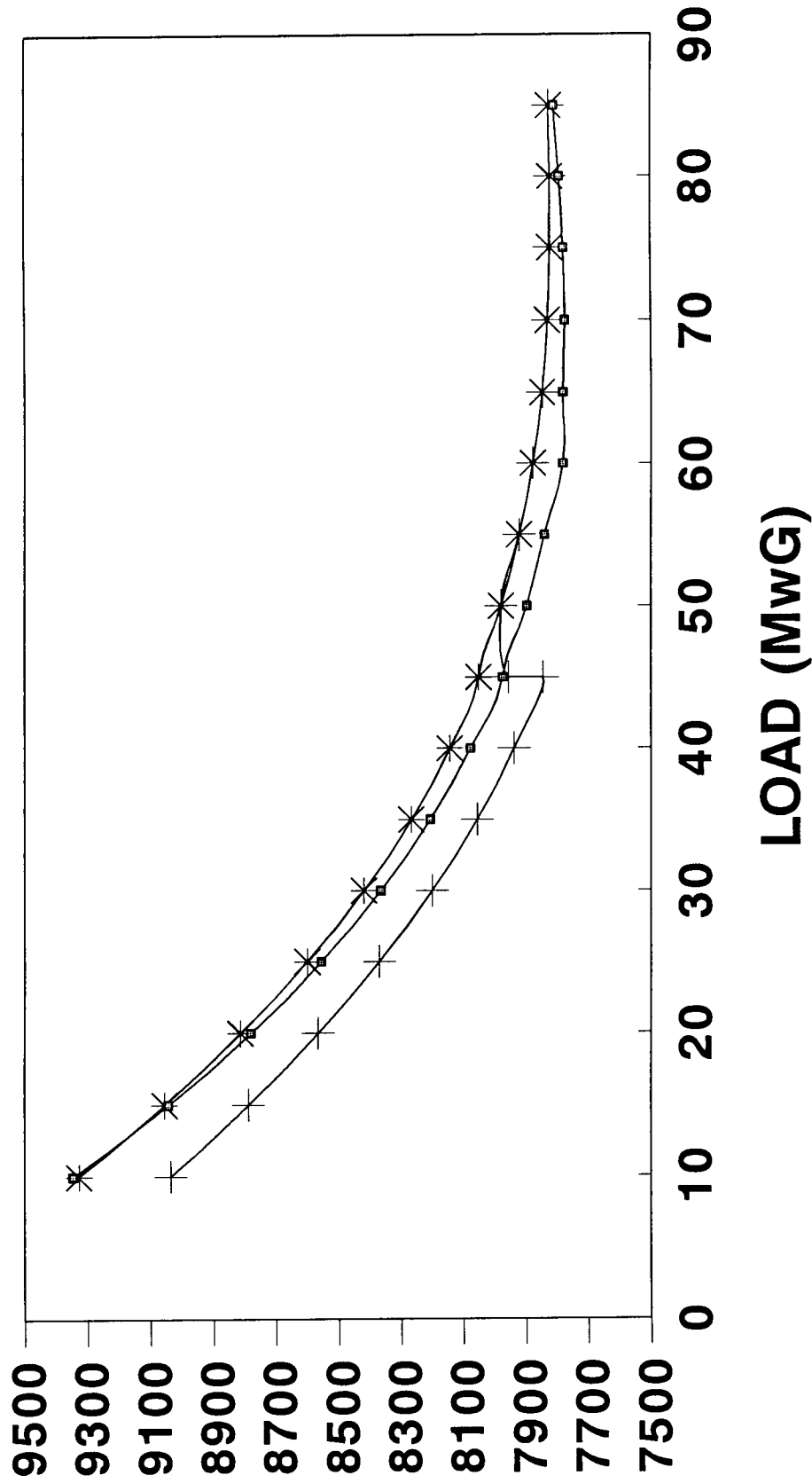


FIGURE 3

—□— BENCHMARK —+— G.S. EFF CONSTANT * G.S. EFF VARIES

UNIT 12 HEAT RATE

FULL SLIDING vs. 4 VALVE HYBRID

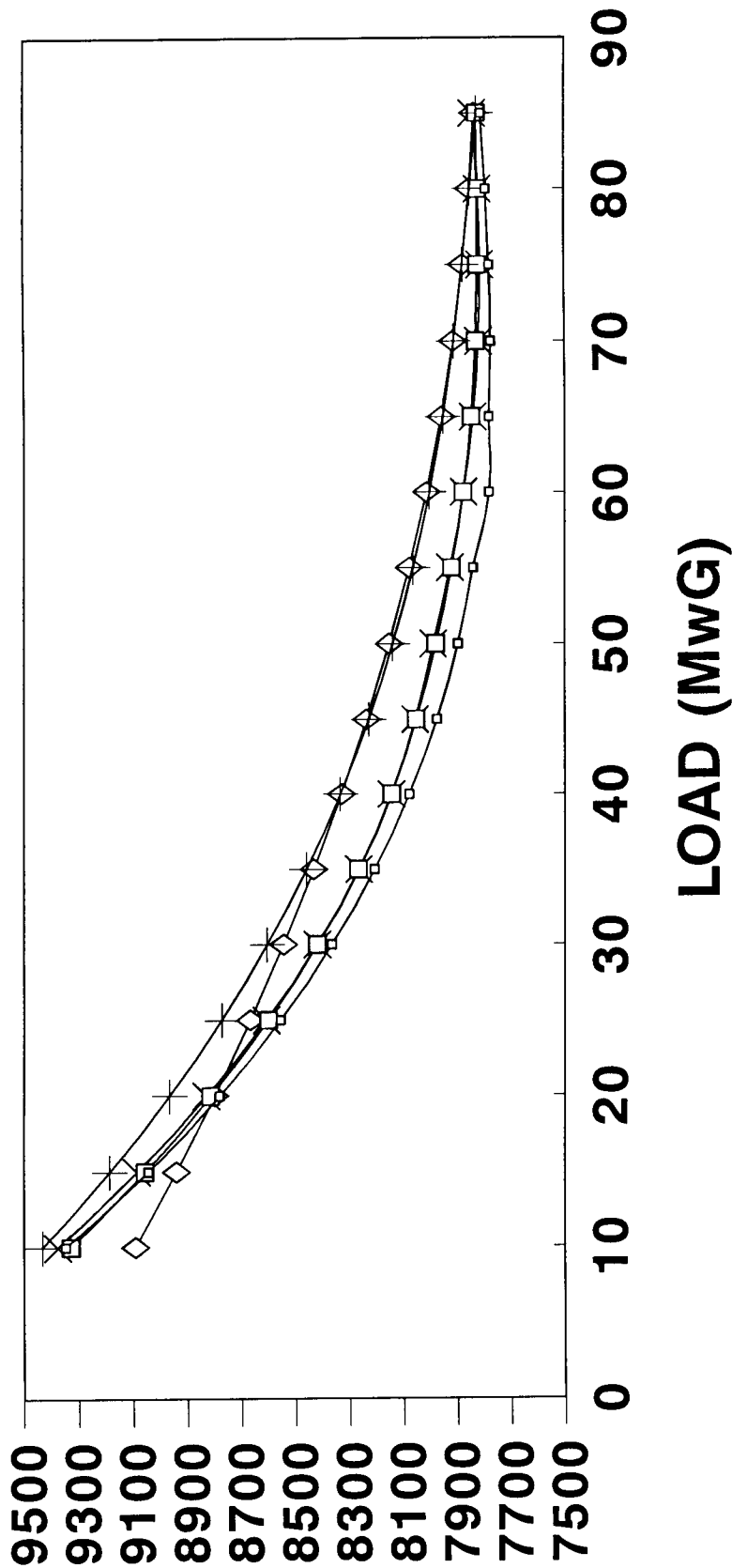


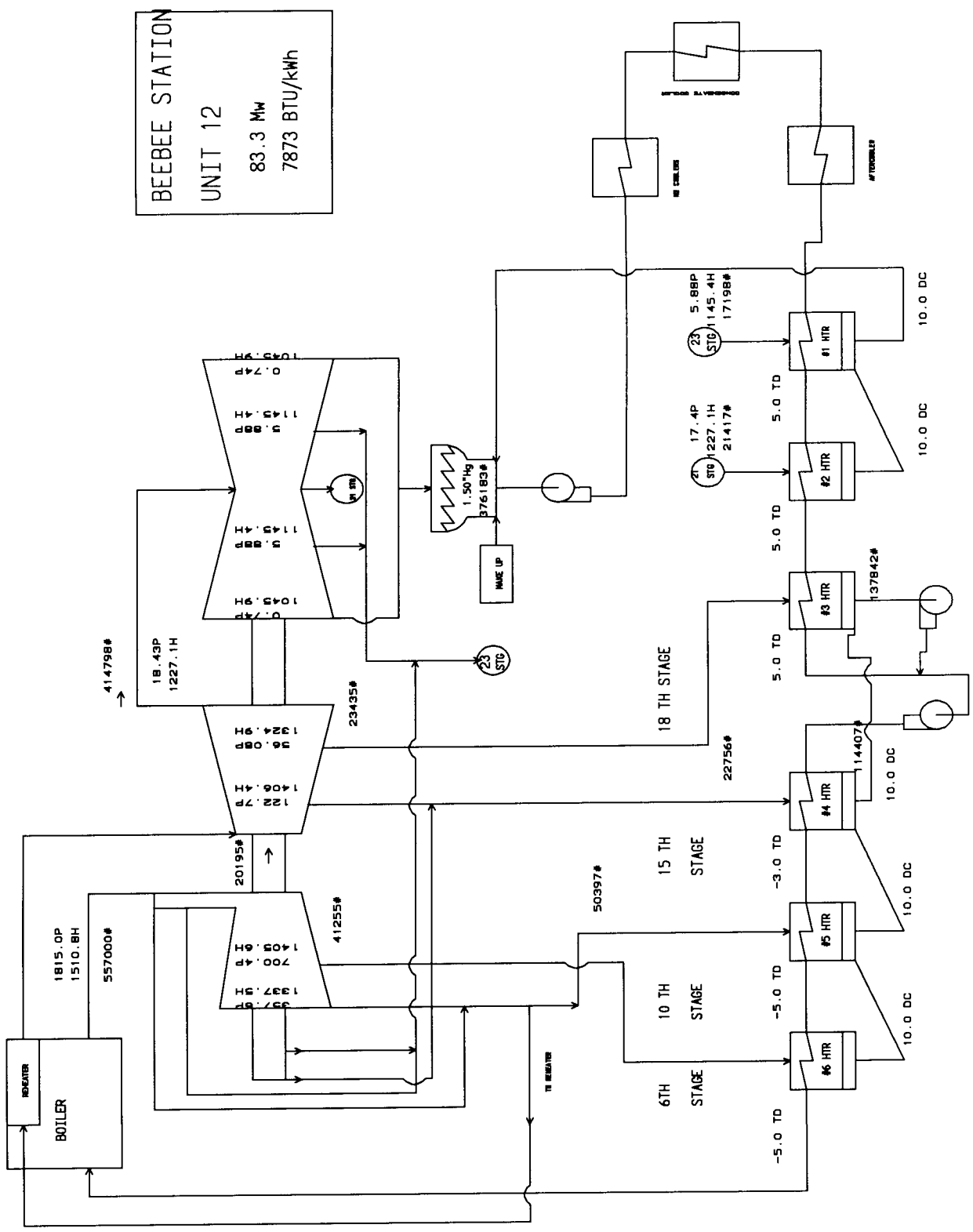
FIGURE 4

- BENCHMARK (TEST)
- +— FULL SLD "A" BFP
- ◇— FULL SLD "B" BFP
- *— HYBRID 4 VLVS "B"
- HYBRID 4 VLVS "A"

BFP OUT AT 61 MWG

Appendix A

321.8P
1525.5H
437299#



BEEBEE STATION
UNIT 12
83.3 MW
7873 BTU/kWh

FILE NAME: 5BEN SLD
RUN DATE: 01/22/90
BENCHMARK B BFP OUT @ 400000#/HR

**
** BEEBEE STATION - UNIT # 12 **
** BENCHMARK CONFIGURATION MODEL **
** (CURRENT PLANT) **
** BUEHLMAN/LITT/O'CONNOR **
** 01/02/90 **

THIS MODEL CONTAINS THE FOLLOWING SCHEDULES :

- (1) HYDROGEN COOLER HEAT INPUT VS. THROTTLE FLOW
- (2) TOTAL GENERATOR ELECTRICAL LOSS VS. GENERATOR GROSS OUTPUT
- (3) GOV. STAGE (30) EFF. MULTIPLIER VS. EQ. THROTTLE FLOW RATIO
- (4) FIRST STAGE I.P.(60) EFF. MULT. VS. HOT REHEAT PRESSURE
- (5) GOV. STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO
- (6) 6TH STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO
- (7) 10TH STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO
- (8) 15TH STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO
- (9) 18TH STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO
- (10) 21ST STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO
- (11) 23RD STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO
- (12) 25TH STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO
- (13) # 6 EXTRACTION PRESSURE DROP CONSTANTS VS. THROTTLE FLOW
- (14) # 5 EXTRACTION PRESSURE DROP CONSTANTS VS. THROTTLE FLOW
- (15) # 3 EXTRACTION PRESSURE DROP CONSTANTS VS. THROTTLE FLOW
- (16) # 2 EXTRACTION PRESSURE DROP CONSTANTS VS. THROTTLE FLOW
- (17) # 1 EXTRACTION PRESSURE DROP CONSTANTS VS. THROTTLE FLOW
- (18) 6TH STAGE SHAPER CONSTANT VS. THROTTLE FLOW
- (19) 15TH STAGE SHAPER CONSTANT VS. THROTTLE FLOW
- (20) 18TH STAGE SHAPER CONSTANT VS. THROTTLE FLOW
- (21) 12-A FEEDWATER PUMP EFFICIENCY VS. FEEDWATER PUMP FLOW
- (22) 12-A FEEDWATER PUMP HEAD VS. FEEDWATER PUMP FLOW
- (23) 12-B FEEDWATER PUMP EFFICIENCY VS. FEEDWATER PUMP FLOW
- (24) 12-B FEEDWATER PUMP HEAD VS. FEEDWATER PUMP FLOW

*
*
*
*
*

***** TABLE SUPPRESSION CARDS *****

SYSTEMS TABLES

* FLAG SETTINGS AND DATA FOR SYSTEM
 * GEOMETRY CONFIGURATION OF MODEL
 * COMPONENT PROPERTIES
 * STREAM PROPERTIES
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 REGENERATOR DESIGN OUTPUT
 * DETAILED SOURCE, SINK, AND VALVE PERFORMANCE OUTPUT
 AND DETAILED THROTTLE VALVE PERFORMANCE OUTPUT
 * DETAILED PUMP PERFORMANCE OUTPUT
 * DETAILED MIXER PERFORMANCE OUTPUT
 * DETAILED SPLITTER PERFORMANCE OUTPUT
 * DETAILED FURNACE / COMBUSTER PERFORMANCE OUTPUT
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 * FIRST LAW OF THERMODYNAMICS PERFORMANCE - SYSTEM
 * SECOND LAW OF THERMODYNAMICS PERFORMANCE - COMPONENTS
 * SECOND LAW OF THERMODYNAMICS PERFORMANCE - STREAMS
 * SECOND LAW OF THERMODYNAMICS PERFORMANCE - SYSTEM
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 * TURBINE EXPANSION CHARACTERISTICS
 * PROPERTIES OF ACTIVE STREAMS

SPECIALIZED TABLES

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 * WARNING TABLE OF STREAM CLOSURES
 * DETAILED NUCLEAR REHEATER DESIGN OUTPUT
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 * CONTROLLED VARIABLE VALUES CALCULATED
 * DEFINITIONS OF SPECIAL OPERATIONS SPECIFIED
 * SPECIAL INPUT VARIABLES, AS SPECIFIED
 * SPECIAL OUTPUT TABLE OF SPECIFIED VARIABLES
 * DETAILED FEEDWATER HEATER DESIGN OUTPUT
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 * OPERATION SET VALUES CALCULATED
 * IORDER ARRAY TABLE AND EORDER ARRAY TABLE
 * DEBUG PRINT OF COMPONENT AND STREAM RESULTS
 * DEBUG PRINT OF COMPONENT AND STREAM RESULTS PLUS
 WARNINGS ASSOCIATED WITH COMPONENT AND STREAM
 DEBUG OUTPUT
 * DEBUG OUTPUT, RUN PARAMETERS RELEVANT TO CONVERGENCE
 * BOILER EFFICIENCY BY HEAT LOSS METHOD
 * DESIGN MODE CONDENSER AND FEEDWATER HEATER DEBUG
 OUTPUT
 * PERFORMANCE TEST ANALYSIS RESULTS (SPECIAL OPTION 6)
 * CALCULATED CONTROL BLOCK GAINS
 * DEBUG OUTPUT COMPONENT TABLE
 * DEBUG OUTPUT STREAM ARRAYS
 * DEBUG OUTPUT COMPONENT ARRAYS
 * ABNORMAL TERMINATION RUN PARAMETERS RELEVANT TO
 CONVERGENCE
 * CONTROL BLOCK STATUS REPORT

***** GENERIC INPUT DATA CARDS *****

*
 *
 011010 1 2 1 0 3600 96000. .85 44.70 44.70
 011011 360. 1190. * VWO
 *

 ***** CONVERGENCE CRITERIA *****

*
 *
 012000 50 50. 50. 0. 0. 0. 0 1.E5
 010200 2 3 1 1 1
 010201 3
 *

 ***** MAIN STREAM DESCRIPTIONS *****

*STREAM	FROM	PORT ID	TO	PORT ID
500050	700,	U,	010,	I
500150	010,	U,	020,	I
500250	020,	U,	030,	I
500350	030,	U,	040,	I
500550	050,	U,	060,	I
500650	060,	U,	070,	I
500750	070,	U,	080,	IA
500850	080,	U,	090,	I
500950	090,	U,	100,	IA
501050	100,	U,	110,	T
501150	110,	T,	120,	I
501250	120,	U,	130,	IA
501650	160,	U,	170,	I
501750	170,	U,	180,	I
501850	180,	U,	190,	S
501950	190,	D,	200,	I
502050	200,	U,	220,	T
502250	220,	T,	230,	T
502350	230,	T,	250,	T
502550	250,	T,	260,	T
502650	260,	T,	270,	T
502750	270,	T,	280,	T
502850	280,	T,	290,	IA
502890	280,	D,	470,	I
504720	470,	U,	290,	IB
502950	290,	U,	300,	IA
503050	300,	B,	305,	I
503070	305,	B,	310,	I
503120	305,	U,	315,	I
503130	310,	U,	800,	IB
503170	315,	U,	800,	IA
503190	800,	U,	320,	I
503250	320,	U,	325,	I
503260	325,	U,	460,	I
503270	460,	U,	450,	I
503280	450,	U,	330,	T
503350	330,	T,	340,	T
503450	340,	T,	350,	T
503550	350,	T,	360,	I

 ***** EXTRACTION STREAM DESCRIPTIONS *****

500910	090,	B,	340,	S
504410	440,	U,	330,	S
501710	170,	E,	430,	IA
504310	430,	U,	260,	S

 ***** DRAIN STREAM DESCRIPTIONS *****

```

*
503590      350,      D,      340,      D
503490      340,      D,      330,      D
503390      330,      D,      280,      D
502790      270,      D,      260,      D
502690      260,      D,      490,      IA
504920      490,      U,      190,      D

```

```

*****
***** MISCELLANEOUS STREAM DESCRIPTIONS *****
*****

```

```

*
500220      020,      B,      400,      I
504030      400,      B,      420,      IB
504020      400,      U,      080,      IB
500420      040,      B,      130,      IB
500710      070,      B,      410,      I
504110      410,      U,      440,      IB
504120      410,      B,      420,      IA
504220      420,      U,      430,      IB
504630      450,      B,      100,      IB
509320      930,      U,      190,      T
501920      190,      T,      920,      I
509420      940,      U,      490,      IB
509620      960,      U,      300,      IB
503220      320,      B,      910,      I
504620      460,      B,      900,      I

```

```

*****
***** EXTRACTION PRESSURE DROP CONSTANTS *****
*****

```

```

*
600540 2 0.0516      * # 6 EXTRACTION
600910 2 0.0503      * # 5 EXTRACTION
604410 2 0.0522      * # 4 EXTRACTION
601540 2 0.0524      * # 3 EXTRACTION
601640 2 0.0549      * # 2 EXTRACTION
604310 2 0.0521      * # 1 EXTRACTION

```

```

*****
***** TURBINE (TYPE 8) *****
*****

```

```

* HIGH PRESSURE TURBINE STAGES

```

```

*
700300 8 1 0 0 1 0 1 3 0.0
700303 0.77898 10207.9
700309 1760.55 1510.79 553371.0

```

```

*
700500 8 1 1 1 2 0 1 3 0.03
700503 0.81974 18708.3

```

```

*
700600 8 1 3 0 2 0 1 1 0.0
700601 0.83112 357.346

```

```

* INTERMEDIATE PRESSURE TURBINE STAGES * IPTYPE DESIGNATED AS LP

```

```

*
701400 8 1 0 1 4 0 1 3 0.03
701403 0.87128 95532.6
701409 315.214 1524.01 457225.0

```

```

*
701500 8 1 1 1 4 0 1 3 0.03
701503 0.85763 183621.0

```

```

*
701600 8 1 1 1 4 0 1 1 0.03
701601 0.87403 18.428

```

```

* LOW PRESSURE TURBINE STAGES

```

```

*
701700 8 1 1 1 4 0 2 3 0.03
701703 0.89719 1257000.0
701709 18.428 1227.16 392716.0

```

```

*
701800 8 1 3 0 4 0 2 1 0.0 0.0 26.175 * GE EXHAUST LOSS

```

701801 0.89413 0.737 * EFF. AT BASE PRESS.

*
*

***** CONDENSER *****

701900 10 1 2 0.0 -1.5

*

***** FEEDWATER HEATERS (PERFORMANCE MODE) *****

*
703500 18 0 050 2 0.0 -5.0 10.0 * # 6 HIGH PRESSURE HEATER
703400 18 1 090 2 0.0 -5.0 10.0 * # 5 HIGH PRESSURE HEATER
703300 18 1 140 2 0.0 -3.0 10.0 * # 4 HIGH PRESSURE HEATER
*
702800 17 1 150 2 0.0 5.0 * # 3 LOW PRESSURE HEATER
702700 16 0 160 2 0.0 5.0 10.0 * # 2 LOW PRESSURE HEATER
702600 16 1 170 2 0.0 5.0 10.0 * # 1 LOW PRESSURE HEATER

*

***** REHEATER *****

701100 25 2 1000.0 .0999

*

***** VALVES *****

*
* THROTTLE VALVE

700100 35 -2.0 -2.0 -2.0 .30 1815.0 1510.9 557000.0 * VWO - 83.270 MWG

* REHEAT VALVE

701200 34 0.02

* FEEDWATER VALVE

703250 34 0.10

*

***** PUMPS *****

* 12-A FEEDWATER PUMP (HYDRAULIC COUPLING)

703100 41 2208.0 0.87 1.0 0.70

* 12-B FEEDWATER PUMP (DIRECT DRIVE)

703150 41 2208.0 0.87 1.0 0.70

* CONDENSATE PUMP

702000 41 245.0

* HEATER DRAIN PUMP

704700 41 245.0

*

***** MIXERS AND SPLITTERS *****

* MIXERS

700800 50 1
 704200 50
 701000 50 1
 701300 50 1
 704400 50 1
 704300 50 1
 703000 50
 702900 50
 704900 50
 708000 50

*
 * SPLITTERS

*
 700400 64 386.635 * PACLEK
 700700 64 505.519 * PACLEK
 700900 60 0.0 50554.0
 704100 64 783.775 * PACLEK
 700200 68 3629.0 57.7267 * PACLEK
 704000 68 643.52.1272 * PACLEK
 704500 61 0.0 0.0
 704600 61 0.0 0.0
 703200 61 0.0 15000.0 * BWCP MAKE-UP
 703050 63 0.0 0.5

*

 ***** SOURCES AND SINKS *****

*
 707000 33 1050.0 1815.0 557000.0 * BOILER - VALVES WIDE OPEN
 709300 31 54.0 26.0 19208448.0 * CIRCULATING WATER - INPUT
 709200 30 * CIRCULATING WATER - OUTPUT
 709400 31 70. 14.7 0.0 * 2875.0 * MAKE-UP
 709100 30 * BWCP INJECTION
 709000 30 * SUPERHEAT SPRAY
 709600 31 288.0 2245.0 12000.0 * BWCP RETURN
 703600 32 * FEEDWATER

*

 ***** HEAT EXCHANGERS *****

*
 * CONDENSATE COOLER

*
 702200 27 0.0

*
 * HYDROGEN COOLER

*
 702300 27 3754300.0

*
 * AFTER COOLER

*
 702500 27 0.0

*

 ***** SCHEDULES *****

*
 * HYDROGEN COOLER HEAT INPUT VS. THROTTLE FLOW

*
 810100 139000. 201000. 265000. 328500. 389000. 442000.
 810101 500500. 557000.
 810110 0.0 388.0 445.0 518.0 596.0 687.0 788.0
 810111 959.0 1100.0
 820100 3412.13
 830100 01, BBHXGR, 230, WW, 005

*
 * TOTAL GENERATOR ELECTRICAL LOSS VS. GENERATOR GROSS OUTPUT

*
 810200 21.530 31.823 42.146 51.979 60.963 68.427 76.202 83.270
 810210 0.0 478. 535. 608. 686. 777. 878. 1049. 1190.
 830200 02, BKELEI, 1, BKGRO, 1

*
 * GOV. STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO

*

810500 0.36083 0.47572 0.58972 0.69833 0.79347 0.89849 1.00000
 810510 0.0 0.40195 0.45493 0.51648 0.58379 0.64753 0.72025 0.77898
 830500 05, EFFTRE, 030, EQTFR, 10

* 6TH STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO

810600 0.36083 0.47572 0.58972 0.69833 0.79347 0.89849 1.00000
 810610 0.0 0.86918 0.86591 0.85199 0.83701 0.82466 0.81791 0.81974
 830600 06, EFFTRE, 050, EQTFR, 10

* 10TH STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO

810700 0.36083 0.47572 0.58972 0.69833 0.79347 0.89849 1.00000
 810710 0.0 0.80048 0.81444 0.82242 0.82906 0.83258 0.83367 0.83112
 830700 07, EFFTRE, 060, EQTFR, 10

* 15TH STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO

810800 0.36083 0.47572 0.58972 0.69833 0.79347 0.89849 1.00000
 810810 0.0 0.88727 0.88146 0.87896 0.87598 0.87363 0.87151 0.87129
 830800 08, EFFTRE, 140, EQTFR, 10

* 18TH STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO

810900 0.36083 0.47572 0.58972 0.69833 0.79347 0.89849 1.00000
 810910 0.0 0.86929 0.86719 0.86445 0.86541 0.86506 0.86214 0.85763
 830900 09, EFFTRE, 150, EQTFR, 10

* 21ST STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO

811000 0.36083 0.47572 0.58972 0.69833 0.79347 0.89849 1.00000
 811010 0.0 0.87604 0.87073 0.87033 0.86748 0.86727 0.86938 0.87403
 831000 10, EFFTRE, 160, EQTFR, 10

* 23RD STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO

811100 0.36083 0.47572 0.58972 0.69833 0.79347 0.89849 1.00000
 811110 0.0 0.89778 0.89628 0.89634 0.89597 0.89598 0.89616 0.89719
 831100 11, EFFTRE, 170, EQTFR, 10

* 25TH STAGE EFFICIENCY VS. EQUIVALENT THROTTLE FLOW RATIO

811200 0.36083 0.47572 0.58972 0.69833 0.79347 0.89849 1.00000
 811210 0.0 0.89686 0.89500 0.89455 0.89390 0.89365 0.89357 0.89414
 831200 12, EFFTRE, 180, EQTFR, 10

* # 6 EXTRACTION PRESSURE DROP CONSTANTS VS. THROTTLE FLOW - STREAM 54

811300 201000. 265000. 328500. 389000. 442000. 500500. 557000.
 811310 0.0 0.0558 0.0551 0.0539 0.0528 0.0520 0.0514 0.0516
 831300 13, PFAC1, 054, WW, 005

* # 5 EXTRACTION PRESSURE DROP CONSTANTS VS. THROTTLE FLOW - STREAM 91

811400 201000. 265000. 328500. 389000. 442000. 500500. 557000.
 811410 0.0 0.0502 0.0503 0.0502 0.0496 0.0497 0.0500 0.0503
 831400 14, PFAC1, 091, WW, 005

* # 4 EXTRACTION PRESSURE DROP CONSTANTS ARE NOT SCHEDULED - STREAM 441

* # 3 EXTRACTION PRESSURE DROP CONSTANTS VS. THROTTLE FLOW - STREAM 154

811500 201000. 265000. 328500. 389000. 442000. 500500. 557000.
 811510 0.0 0.0503 0.0513 0.0526 0.0512 0.0514 0.0514 0.0524
 831500 15, PFAC1, 154, WW, 005

* # 2 EXTRACTION PRESSURE DROP CONSTANTS VS. THROTTLE FLOW - STREAM 164

811600 201000. 265000. 328500. 389000. 442000. 500500. 557000.
 811610 0.0 0.0528 0.0562 0.0537 0.0497 0.0502 0.0523 0.0549
 831600 16, PFAC1, 164, WW, 005

* # 1 EXTRACTION PRESSURE DROP CONSTANTS VS. THROTTLE FLOW - STREAM 431

811700 201000. 265000. 328500. 389000. 442000. 500500. 557000.
 811710 0.0 0.0531 0.0512 0.0562 0.0514 0.0525 0.0532 0.0521
 831700 17, PFAC1, 431, WW, 005

* 6TH STAGE SHAPER CONSTANT VS. THROTTLE FLOW

811800 201000. 265000. 328500. 389000. 442000. 500500. 557000.
 811810 0.0 443.57 487.10 551.29 650.00 804.58 1029.32 860.27
 831800 18, SHAPER, 50, WW, 005

* 15TH STAGE SHAPER CONSTANT VS. THROTTLE FLOW

811900 201000. 265000. 328500. 389000. 442000. 500500. 557000.
 811910 0.0 550.74 549.18 548.39 549.35 552.32 555.91 558.09
 831900 19, SHAPER, 140, WW, 005

* 18TH STAGE SHAPER CONSTANT VS. THROTTLE FLOW

812000 201000. 265000. 328500. 389000. 442000. 500500. 557000.
 812010 0.0 592.18 584.94 586.95 581.32 582.43 591.09 606.16
 832000 20, SHAPER, 150, WW, 005

* 12-A FEEDWATER PUMP EFFICIENCY VS. FEEDWATER PUMP FLOW

812100 89767.0 112208.0 134650.0 157092.0 179533.0 201975.0 224417.0
 812110 0.0 0.365 0.436 0.488 0.532 0.572 0.610 0.645
 812101 246858.0 269300.0 291745.0 314187.0 336629.0 359071.0 381513.0
 812111 0.675 0.695 0.713 0.723 0.730 0.736 0.730
 812102 403955.0 426397.0 448839.0
 812112 0.726 0.722 0.720
 832100 21, EFFPMP, 310, WW, 313

* 12-A FEEDWATER PUMP HEAD VS. FEEDWATER PUMP FLOW

812200 89767.0 112208.0 134650.0 157092.0 179533.0 201975.0 224417.0
 812210 0.0 2394.0 2380.0 2373.0 2363.0 2352.0 2332.0 2303.0
 812201 246858.0 269300.0 291745.0 314187.0 336629.0 359071.0 381513.0
 812211 2270.0 2237.0 2208.0 2156.0 2105.0 2053.0 1991.0
 812202 403955.0 426397.0 448839.0
 812212 1940.0 1868.0 1795.0
 832200 22, PMPDIS, 310, WW, 313

* 12-B FEEDWATER PUMP EFFICIENCY VS. FEEDWATER PUMP FLOW

812300 0.0 22442.0 44884.0 67326.0 89767.0 112208.0 134650.0
 812310 0.0 0.0 0.110 0.205 0.290 0.370 0.435 0.495
 812301 157092.0 179533.0 201975.0 224417.0 246858.0 269300.0 291745.0
 812311 0.550 0.595 0.630 0.660 0.680 0.700 0.715
 812302 314187.0 336629.0 359071.0 381513.0 403955.0 426397.0
 812312 0.725 0.730 0.738 0.740 0.742 0.740
 832300 23, EFFPMP, 315, WW, 317

* 12-B FEEDWATER PUMP HEAD VS. FEEDWATER PUMP FLOW

812400 44883.0 67325.0 89767.0 112208.0 134650.0 157092.0 179533.0
 812410 0.0 2404.0 2394.0 2390.0 2383.0 2380.0 2361.0 2252.0
 812401 201975.0 224417.0 246858.0 269300.0 291745.0 314187.0 336629.0
 812411 2332.0 2303.0 2270.0 2229.0 2208.0 2163.0 2117.0
 812402 359071.0 381513.0 403955.0 426397.0
 812412 2043.0 1981.0 1909.0 1816.0
 832400 24, PMPDIS, 315, WW, 317

 ***** SPECIAL OUTPUT VARIABLES *****

*
 *
 890010 'GROSS TURBINE CYCLE POWER OUTPUT (MW)'
 890011 BKGROS, 0

* OPERATION TO CALCULATE THE GROSS TURBINE CYCLE HEAT RATE

*
 870080 1000. * MW TO KW CONVERSION
 880010 HH, 005, SUB, HH, 355, OPVB, 10
 880020 OPVB, 10, MUL, WW, 005, OPVB, 11
 880030 HH, 115, SUB, HH, 105, OPVB, 12
 880040 OPVB, 12, MUL, WW, 115, OPVB, 13
 880050 OPVB, 11, ADD, OPVB, 13, OPVB, 14
 880060 OPVB, 14, DIV, BKGROS, 1, OPVB, 15
 880070 OPVB, 15, DIV, OPVB, 8, OPVB, 16

*
 890020 'GROSS TURBINE CYCLE HEAT RATE (BTU/KWH)'
 890021 OPVB, 16

* OPERATION TO CALCULATE THE GROSS TURBINE CYCLE

* THERMAL EFFICIENCY BASED ON OPVB 16 ABOVE
 *
 870330 3412.1416 * KW THERMAL CONVERSION FACTOR
 880080 OPVB, 33, DIV, OPVB, 16, OPVB, 34
 *
 * OPERATION TO CONVERT CYCLE THERMAL EFFICIENCY TO PERCENT
 *
 870980 100. * CONVERSION TO PERCENT
 880090 OPVB, 34, MUL, OPVB, 98, OPVB, 35
 *
 * OPERATION TO CALCULATE INTERMEDIATE PRESSURE SECTION EFFICIENCY
 *
 880100 HH, 115, SUB, HH, 165, OPVB, 39
 880110 PP, -165, PSH, SS, 115, OPVB, 40
 880120 HH, 115, SUB, OPVB, 40, OPVB, 41
 880130 OPVB, 39, DIV, OPVB, 41, OPVB, 42
 *
 * OPERATION TO CALCULATE LOW PRESSURE SECTION EFFICIENCY
 *
 880140 HH, 165, SUB, HH, 185, OPVB, 43
 880150 PP, -185, PSH, SS, 165, OPVB, 44
 880160 HH, 165, SUB, OPVB, 44, OPVB, 45
 880170 OPVB, 43, DIV, OPVB, 45, OPVB, 46
 *
 * OPERATION TO CONVERT HIGH PRESSURE SECTION EFFICIENCY TO PERCENT
 *
 880180 EFFSEC, 060, MUL, OPVB, 98, OPVB, 36
 *
 * OPERATION TO CONVERT INT. PRESSURE SECTION EFFICIENCY TO PERCENT
 *
 880190 OPVB, 42, MUL, OPVB, 98, OPVB, 37
 *
 * OPERATION TO CONVERT LOW PRESSURE SECTION EFFICIENCY TO PERCENT
 *
 880200 OPVB, 46, MUL, OPVB, 98, OPVB, 38
 *
 890030 'GROSS TURBINE CYCLE THERMAL EFFIC. (%)'
 890031 OPVB, 35
 *
 890040 'H.P. TURBINE SECTION EFFIC. (%)'
 890041 OPVB, 36
 *
 890050 'I.P. TURBINE SECTION EFFIC. (%)'
 890051 OPVB, 37
 *
 890060 'L.P. TURBINE SECTION EFFIC. (%)'
 890061 OPVB, 38
 *
 890070 'MAIN STEAM FLOW (#/HR)'
 890071 WW, 005
 *
 890080 'MAIN STEAM PRESSURE (PSIA)'
 890081 PP, 005
 *
 890090 'MAIN STEAM TEMPERATURE (DEG-F)'
 890091 TT, 005
 *
 890100 '1ST STAGE PRESSURE (PSIA)'
 890101 PP, 035
 *
 890110 '10TH STAGE PRESSURE (PSIA)'
 890111 PP, 065
 *
 890120 'COLD REHEAT PRESSURE (PSIA)'
 890121 PP, 095
 *
 890130 'COLD REHEAT TEMPERATURE (DEG-F)'
 890131 TT, 095
 *
 890140 'HOT REHEAT PRESSURE (PSIA)'
 890141 PP, 115
 *
 890150 'HOT REHEAT TEMPERATURE (DEG-F)'
 890151 TT, 115
 *
 890160 'I.P. INLET PRESSURE (PSIA)'
 890161 PP, 136
 *
 890170 'I.P. EXHAUST PRESSURE (PSIA)'
 890171 PP, 165

```

*
890180 'CONDENSER BACK PRESSURE           (IN-HG)'
890181 PP, 195
*
890190 'CIRC. WATER INLET TEMPERATURE     (DEG-F)'
890191 TT, 932

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*****
***** SPECIAL INPUT VARIABLES *****
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*
890200 '12-A FEEDWATER PUMP MOTOR POWER   (KW)'
*890201 BKPMOT, 310, 929.0, I
*
890210 '12-B FEEDWATER PUMP MOTOR POWER   (KW)'
*890211 BKPMOT, 315, 895.0, I
*
890220 '# 6 HEATER F.W. PRESSURE DROP      (PSIA)'
890221 PDFW, 350, 12.0, I
*
890230 '# 5 HEATER F.W. PRESSURE DROP      (PSIA)'
890231 PDFW, 340, 7.9, I
*
890240 '# 4 HEATER F.W. PRESSURE DROP      (PSIA)'
890241 PDFW, 330, 13.8, I
*
890250 '# 3 HEATER F.W. PRESSURE DROP      (PSIA)'
890251 PDFW, 280, 11.6, I
*
890260 '# 2 HEATER F.W. PRESSURE DROP      (PSIA)'
890261 PDFW, 270, 14.4, I
*
890270 '# 1 HEATER F.W. PRESSURE DROP      (PSIA)'
890271 PDFW, 260, 6.0, I

```

```

*
890000 1 1 * OUTPUT FORMAT CONTROL FOR FLOATING POINT
*
020000 PRINT NOPRNT * SUPPRESSION OF 80 COLUMN PC OUTPUT
*
010002 1 * 132 COLUMN PC FORMAT

```

```

*****
***** TIP LEAKAGE GEOMETRY *****
*****

```

```

* 6TH STAGE

```

```

500450 040, U, 001, I
500460 001, U, 050, I
500470 001, B, 011, IB
500510 050, E, 011, IA
500540 011, U, 350, S

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* 15TH STAGE

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```

501350 130, U, 002, I
501360 002, U, 140, I
501370 002, B, 021, IB
501410 140, E, 021, IA
501440 021, U, 440, IA

```

```

* 18TH STAGE

```

```

501450 140, U, 003, I
501460 003, U, 150, I
501470 003, B, 031, IB
501510 150, E, 031, IA
501540 031, U, 280, S

```

```

* 21ST STAGE

```

```

501550 150, U, 004, I
501560 004, U, 160, I
501570 004, B, 041, IB
501610 160, E, 041, IA

```

501640 041, U, 270, S

*
*

***** TIP LEAKAGE MIXERS AND SPLITTERS *****

* MIXERS

*
700110 50 1
700210 50 1
700310 50 1
700410 50 1

* SPLITTERS

*
700010 61 0.0 0.0
700020 61 0.0 0.0
700030 61 0.0 0.0
700040 61 0.0 0.0

*

***** REPLACEMENT CARDS FOR VARIABLE LOAD CONDITIONS *****

/
= BEEBEE STATION - UNIT # 12 - 500500 #/HR FLOW - 76.202 MW - GROSS

*
707000 33 1050. 1815. 500500.
*709400 31 70. 14.7 2502.
011010 1 2 1 0 3600 96000. 0.85 44.7 32.2

/
= BEEBEE STATION - UNIT # 12 - 442000 #/HR FLOW - 68.427 MW - GROSS

*
707000 33 1050. 1815. 442000.
*709400 31 70. 14.7 2210.
011010 1 2 1 0 3600 96000. 0.85 44.7 20.4

/
= BEEBEE STATION - UNIT # 12 - 389000 #/HR FLOW - 60.963 MW - GROSS

*
707000 33 1050. 1815. 389000.
703050 63 0.0 0.0
*709400 31 70. 14.7 1945.
011010 1 2 1 0 3600 96000. 0.85 44.7 15.2

/
= BEEBEE STATION - UNIT # 12 - 328500 #/HR FLOW - 51.979 MW - GROSS

*
707000 33 1050. 1815. 328500.
*709400 31 70. 14.7 1642.
011010 1 2 1 0 3600 96000. 0.85 44.7 15.2

/
= BEEBEE STATION - UNIT # 12 - 265000 #/HR FLOW - 42.146 MW - GROSS

*
707000 33 1050. 1815. 265000.
*709400 31 70. 14.7 1325.
011010 1 2 1 0 3600 96000. 0.85 44.7 15.2

/
= BEEBEE STATION - UNIT # 12 - 201000 #/HR FLOW - 31.823 MW - GROSS

*
707000 33 1050. 1815. 201000.
*709400 31 70. 14.7 1005.
011010 1 2 1 0 3600 96000. 0.85 44.7 15.2

*/
= BEEBEE STATION - UNIT # 12 - 139000 #/HR FLOW - 21.530 MW - GROSS

* NOTE: IN THE THERMAL KIT HEAT BALANCE THE EXTRACTION
* FLOW TO # 1 FEEDWATER HEATER DOES NOT OBEY THE FIRST
* LAW OF THERMODYNAMICS AND WILL NOT CONVERGE.

*
*707000 33 1050. 1815. 139000.
*709400 31 70. 14.7 695.

```

/
*
= SPECIAL OPTION 1 TO SET FLOW CAPACITY 4 VLVS OPEN
850000 1
700101 1815. 1510.7855 328500.
700109 1815. 1510.7855 178.22
891981 PPVSC 700 1500. I
700100 35 -2.0 .03 -2.0 .361 1815.0 1510.9 557000.0 * SET ADMISSION
* EQUIVALENT THROTTLE FLOW RATIO TO 4 VALVES OPEN. ASSUMED TO BE
* HALF LOAD. NO DOCUMENTATION AVAILABLE.
/
= PRESSURE LOWERED TO 1425 PSIA. DIRECT DRIVE PUMP OUT
020001 PRINT * FLAG SETTINGS AND DATA FOR SYSTEM
020003 PRINT * COMPONENT PROPERTIES
020006 PRINT * DETAILED TURBINE PERFORMANCE OUTPUT - TABLE A
020007 PRINT * DETAILED TURBINE PERFORMANCE OUTPUT - TABLE B
020008 PRINT * DETAILED TURBINE PERFORMANCE OUTPUT - TABLE C
020009 PRINT * DETAILED FEEDWATER HEATER PERFORMANCE OUTPUT - TABLE A
020010 PRINT * DETAILED FEEDWATER HEATER PERFORMANCE OUTPUT - TABLE B
020014 PRINT * DETAILED PUMP PERFORMANCE OUTPUT
020020 PRINT * FIRST LAW OF THERMODYNAMICS PERFORMANCE - SYSTEM
020026 PRINT * TURBINE EXPANSION CHARACTERISTICS
020028 PRINT * PROPERTIES OF ACTIVE STREAMS
020038 PRINT * SPECIAL INPUT VARIABLES, AS SPECIFIED
020039 PRINT * SPECIAL OUTPUT TABLE OF SPECIFIED VARIABLES
* WARNINGS ASSOCIATED WITH COMPONENT AND STREAM
* DEBUG OUTPUT
*= SPECIAL OPTION 3 TO EVALUATE CHANGE IN FLOW
*
*850000 3
*011010 1 2 1 0 3600 96000. .85 44.70 44.70 42500.
891981 PPVSC 700 1425. I
891971 WWVSC 700 201000. I
703050 63 0.0 0.0
*
/
= PRESSURE REDUCED TO 1200 PSIA
891981 PPVSC 700 1200. I
*
.

```